



ROS-based Toolbox for Motor Parameter Identification of Robotic Manipulators

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Premise of study

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■ Complexity vs utility



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- Complexity vs utility
- Availability of parameters



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- Complexity vs utility
- Availability of parameters
- Physical systems discrepancies



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- Identify torque-current and friction coefficients in robot manipulators



Objectives

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- Identify torque-current and friction coefficients in robot manipulators
- Open-source toolbox of the procedure



General Dynamic Model

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- Standard Denavit-Hartenberg kinematic convention [1]



General Dynamic Model

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- Standard Denavit-Hartenberg kinematic convention [1]
- General dynamic model of robot manipulator [2]

$$\tau_m - \tau_{ext} - \tau_{dist} - \tau_f = M(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) \quad (2.1)$$

where $q = [q_1, q_2, q_3, \dots, q_n]^T$ are joint positions and \dot{q} and \ddot{q} are joint velocities and accelerations respectively, while τ are forces/moments of the robot.



Case study on the UR5 (Universal Robots, Odense, Denmark)

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Figure 2.1: Installed UR5

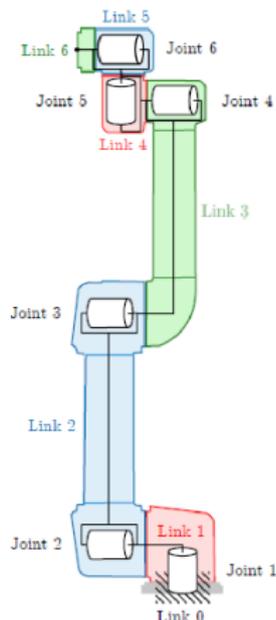


Figure 2.2: Schematic of the UR5



Simplified Dynamic Model

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Equation for the motor torque current relationship [3]

$$\tau_m = k_{ct}i \quad (2.2)$$

Friction model [4]

$$\tau_f = k_{fc}sign(\dot{q}) + k_{fv}\dot{q} \quad (2.3)$$

where $i = [i_1, \dots, i_n]^T$ represent joint currents.



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- Constant velocity, no acceleration influence



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- Constant velocity, no acceleration influence
- No end-effector applied forces during experiments



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- Constant velocity, no acceleration influence
- No end-effector applied forces during experiments
- No disturbances during experiments



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- Constant velocity, no acceleration influence
- No end-effector applied forces during experiments
- No disturbances during experiments
- One joint at a time, minimal joint cross-correlation



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Model used in identification process

$$k_{ct}i = C(q, \dot{q})\dot{q} + G(q) + k_{fc}sign(\dot{q}) + k_{fv}\dot{q} \quad (2.4)$$

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Model used in identification process

green - constant values in one experiment

pink - coefficients to find by fitting

$$k_{ct}i = C(q, \dot{q})\dot{q} + G(q) + k_{fc}sign(\dot{q}) + k_{fv}\dot{q} \quad (2.5)$$

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Model used in identification process

green - constant values in one experiment

pink - coefficients to find by fitting

$$k_{ct} \ddot{i} = C(q, \dot{q})\dot{q} + G(q) + \underbrace{k_{fc} \text{sign}(\dot{q}) + k_{fv}\dot{q}}_{\tau_f} \quad (2.6)$$



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$$\tau_f = k_{fc} \text{sign}(\dot{q}) + k_{fv} \dot{q} \quad (2.7)$$



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- Special cases for joints 1 and 6, for $G(q)$

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- Special cases for joints 1 and 6, for $G(q)$

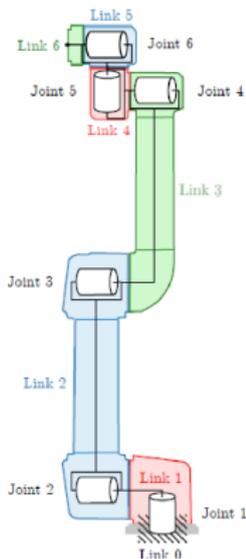


Figure 2.3: UR5 schematic



Figure 2.4: Joint 6 additional mass

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- 1 The identification of torque-current coefficient k_{ct} and the total friction torque τ_f
- 2 The identification of viscous k_{fv} and Coulomb friction parameters k_{fc}
- 3 The analysis of all acquired data to find a triplet $(k_{ct}; k_{fv}; k_{fc})$ as the conclusive parameters for each joint.



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- 1 The identification of torque-current coefficient k_{ct} and the total friction torque τ_f

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- 1 The identification of torque-current coefficient k_{ct} and the total friction torque τ_f (m being the measurement and n the timestep)

$$i_{mn} = \tau_{fmn} + \frac{G_{mn} + C_{mn}\dot{q}_m}{k_{ct}} \quad (3.1)$$

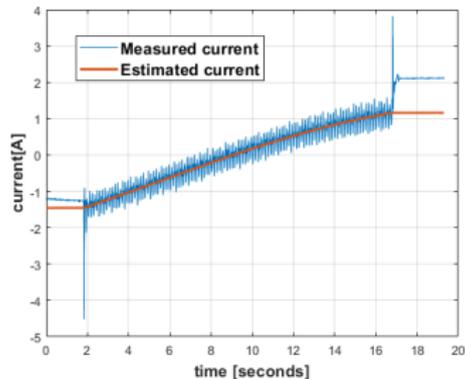


Figure 3.1: Sample of current fitting

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2 The identification of Coulomb k_{fc} and viscous k_{fv} friction parameters

$$\tau_f = k_{fc} \operatorname{sign}(\dot{q}_m) + k_{fv} \dot{q}_m \quad (3.2)$$

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- 3 The processing of all acquired data to find a triplet (k_{ct} ; k_{fv} ; k_{fc}) as the conclusive parameters for each joint. The k_{ct} set found has to be averaged for each velocity in order to apply the fitting for the friction coefficients.

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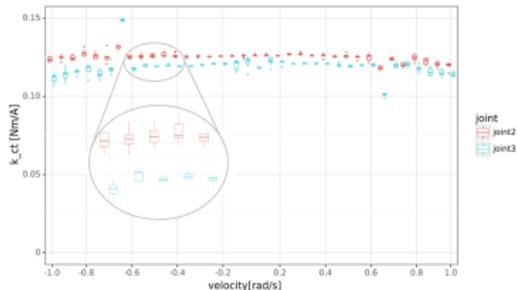


Figure 4.1: The current-torque coefficient (k_{ct}) comparison for the 2nd and 3rd joint

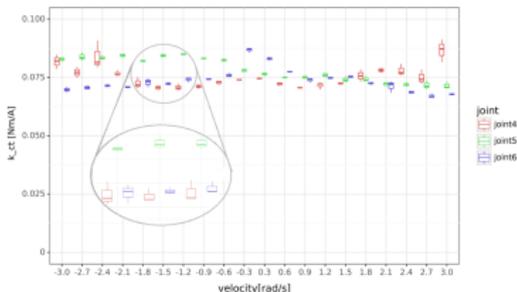


Figure 4.2: The current-torque coefficient (k_{ct}) comparison for the last 3 joints

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$$\tau_f = k_{fc} \text{sign}(\dot{q}) + k_{fv} \dot{q} \quad (4.1)$$

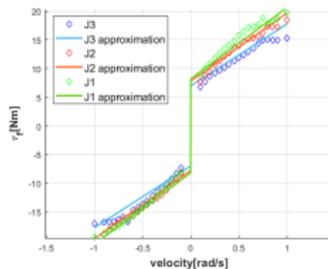


Figure 4.3: The friction term (τ_f) comparison for the first 3 joints

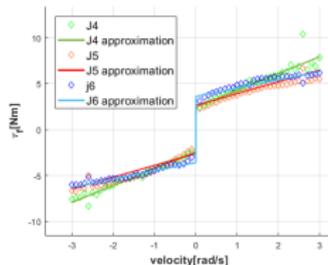


Figure 4.4: The friction term (τ_f) comparison for the last 3 joints

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Table 1: Final values for the identified torque-current k_{ct} , viscous k_{fv} , and Coulomb k_{fc} coefficients

Joint	k_{ct}	k_{fv}	k_{fc}
1	12.3	8.1272	12.3141
2	12.6351	7.7891	11.881
3	12.0383	6.9762	10.7667
4	7.7366	2.4405	1.8286
5	7.9228	2.6265	1.2794
6	7.4723	3.6058	0.8921

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1 Low variability for each separate joint

Table 1: Final values for the identified torque-current k_{ct} , viscous k_{fv} , and Coulomb k_{fc} coefficients

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- 1 Low variability for each separate joint
- 2 Particularity of each joint

Table 1: Final values for the identified torque-current k_{ct} , viscous k_{fv} , and Coulomb k_{fc} coefficients

Joint	k_{ct}	k_{fv}	k_{fc}
1	12.3	8.1272	12.3141
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Example Movie

00:00

*found at <https://gitlab.utcluj.ro/true-rehab/robot-identification>

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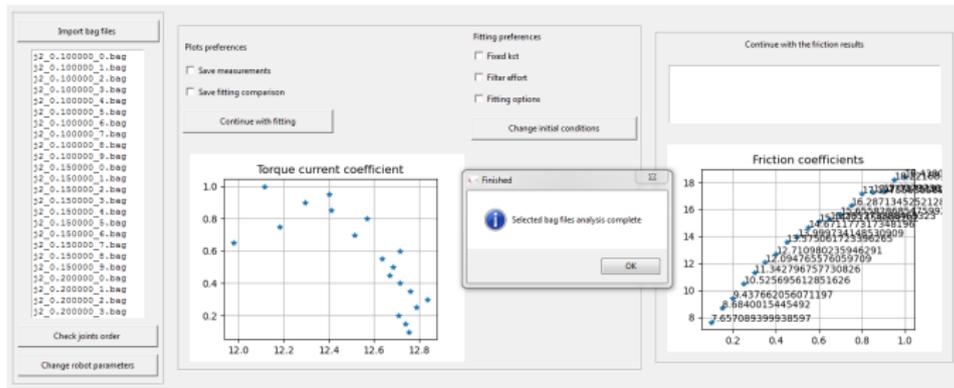


Figure 5.1: Results of the identification

*found at <https://gitlab.utcluj.ro/true-rehab/robot-identification>



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- Higher accuracy in simulations and analysis
- Helpful in model-based control
- Simple enough to easily be implemented by other parties, complex enough to catch main features



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- [2] "Robot Manipulator Control", F. L. Lewis, D. M. Dawson, and C. Abdallah, 2003
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- [4] "A survey and comparison of several friction force models, for dynamic analysis of multibody mechanical systems", F. Marques, P. Flores, J. C. P. Claro and H. M. Lankarani, Nonlinear Dynamics, volume 86, 1407-1443, 2016

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